

Workshop on Multi-body Dynamics

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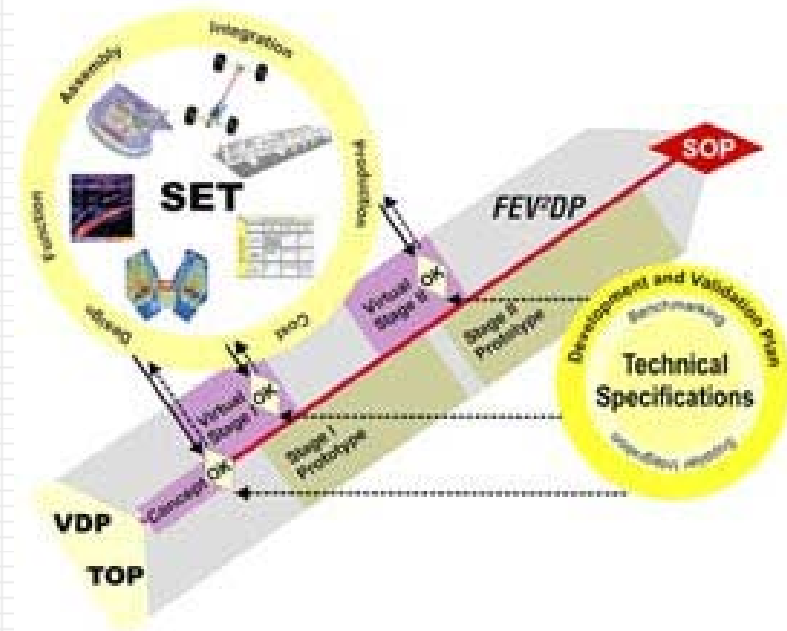
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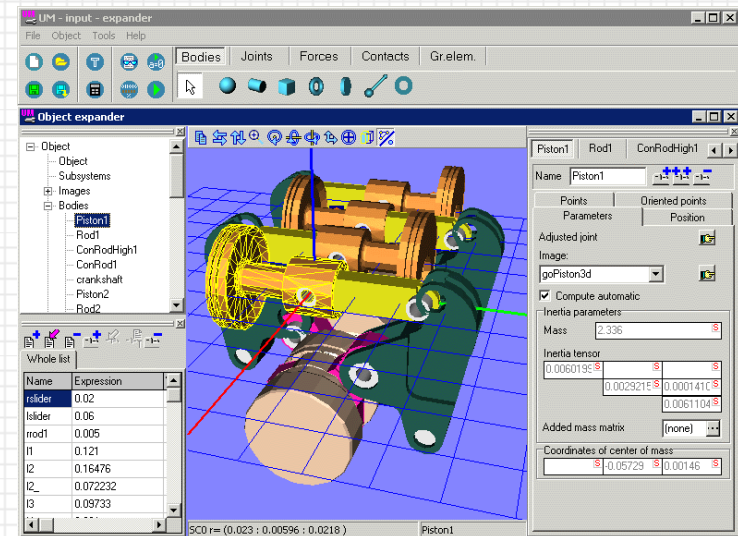
Virtual product development

- **Multibody system:** mechanical system which is mobile or has mobile parts.
- **Multibody dynamics:**
 - Computer simulation of the dynamics of multibody systems.
 - It belongs to the general concept of virtual product development.
- **Advantages:**
 - Anticipation of system behavior during the first stages of the design process.
 - Reduction of physical prototypes and experimental tests.
 - Consequences: higher quality, lower cost, earlier in the market.

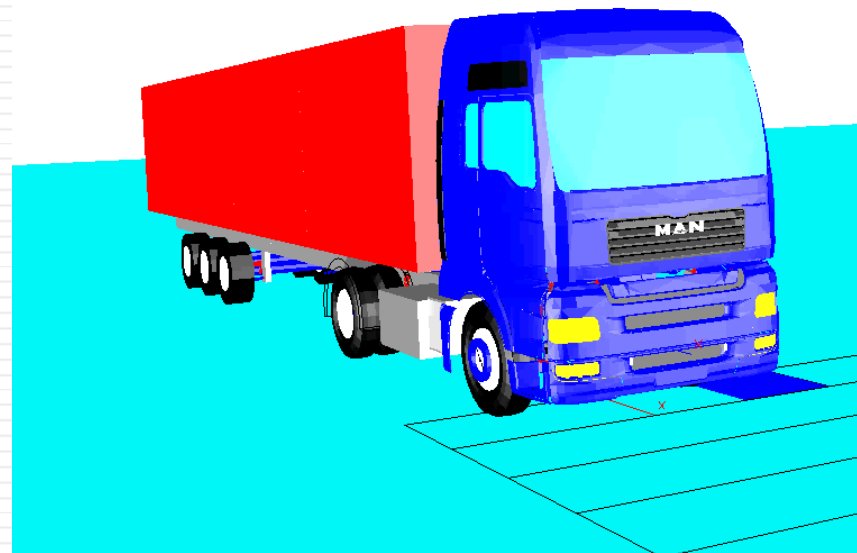
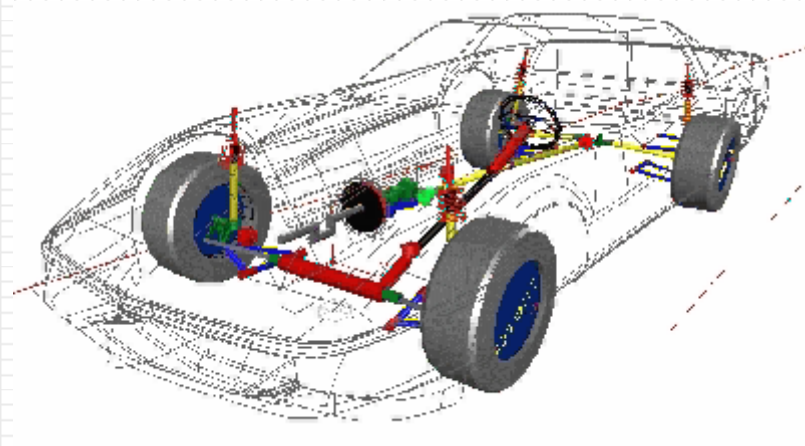


Multibody dynamics

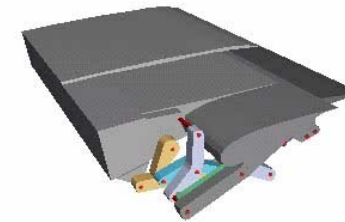
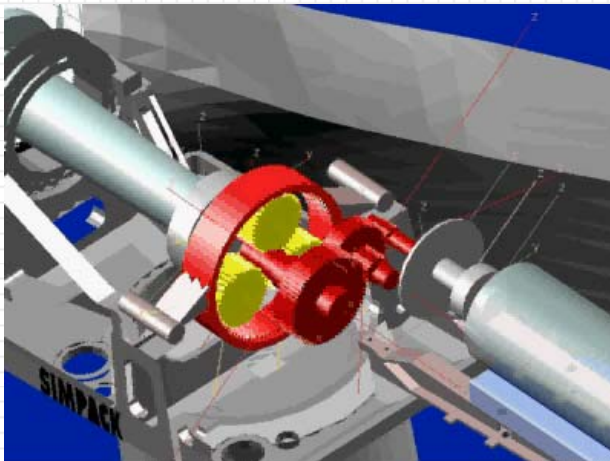
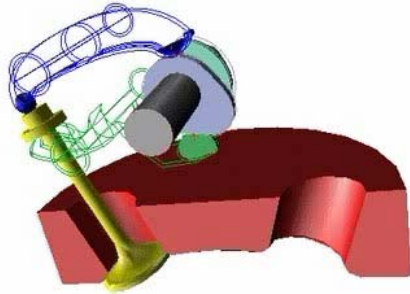
- Computational mechanics of machines and mechanisms: mechanics + numerical methods + programming.
- Enables to solve in the computer the forward dynamics (and the kinematics, and the inverse dynamics) of models of vehicles, machines and mechanisms as detailed as desired.
- Industrial fields of application:
 - Automotive, Aerospace, Railway, Naval, Energy, Heavy Machinery, Machine-Tool, Robotics, Biomechanics, Health, Sports, Entertaining, etc.
- Application in all the stages of the design process:
 - Design, Simulation, Analysis, Control, Test, Manufacturing and Maintenance.



Examples



Examples



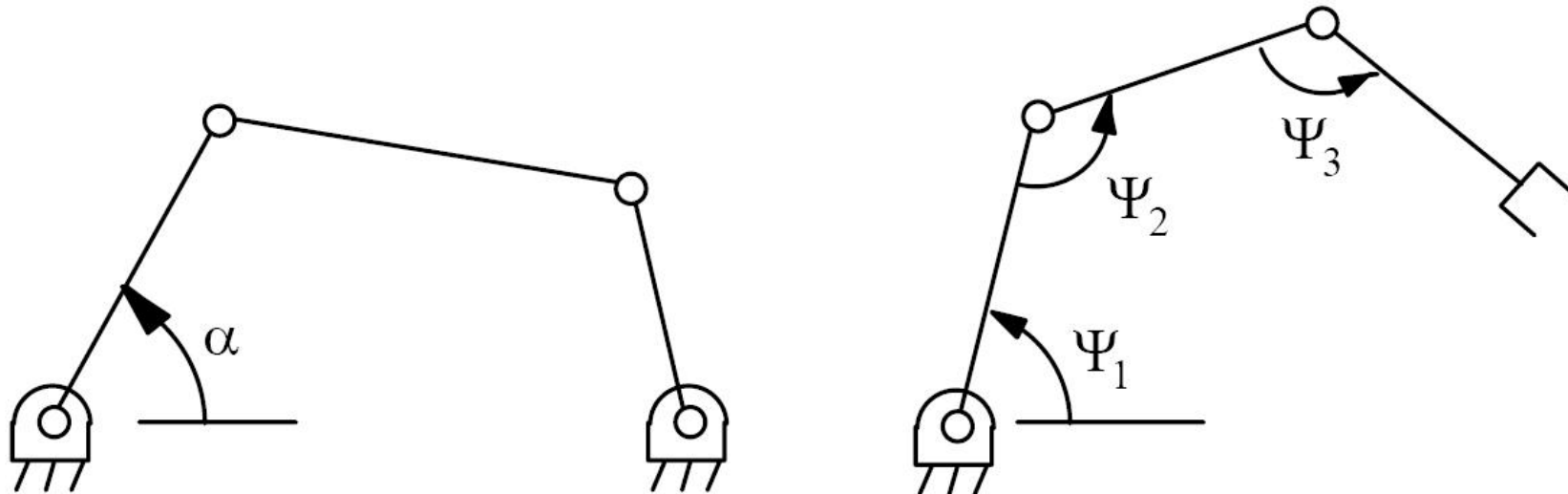
Stages of the multibody dynamics problem

- Problem stages:
 - Physical modeling: simplifications, theories for flexibility, contact, etc.
 - Coordinates selection.
 - Formulation of the equations of motion: kinematics and dynamics.
 - Numerical integration.
 - Implementation: Fortran, C++, Matlab.
- Basic topics:
 - Modeling.
 - Kinematics.
 - Dynamics.



Modeling: traditional method

- Traditionally, mechanisms are modeled in minimum coordinates (Classical Mechanics, Theory of Machines).
- Minimum coordinates: as many as the system degrees of freedom (independent).
- Closed loops are problematic.



Modeling: computational method

- Dependent coordinates: more than the system degrees of freedom.
- Related through constraint equations.

n: number of coordinates

g: number of system degrees of freedom

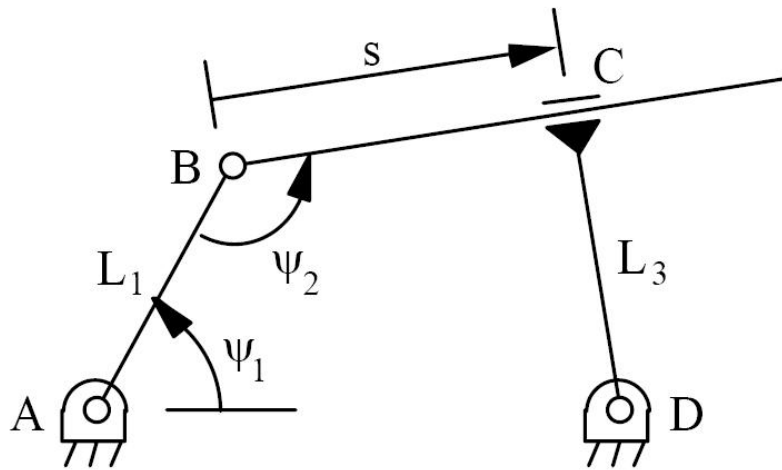
m: number of constraint equations

$$m=n-g$$

- Three families: relative, reference point, natural.



Modeling: relative coordinates

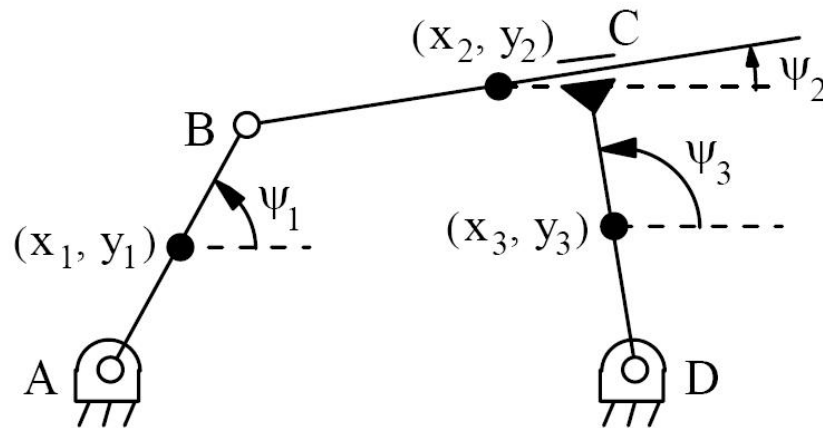


$$\mathbf{AB} + \mathbf{BC} + \mathbf{CD} - \mathbf{AD} = \mathbf{0}$$

$$L_1 \cos \psi_1 + s \cos(\psi_1 + \psi_2 - \pi) + L_3 \sin(\psi_1 + \psi_2 - \pi) - L_4 = 0$$

$$L_1 \sin \psi_1 + s \sin(\psi_1 + \psi_2 - \pi) - L_3 \cos(\psi_1 + \psi_2 - \pi) = 0$$

Modeling: reference point coordinates



$$(x_1 - x_A) - \frac{L_1}{2} \cos \psi_1 = 0$$

$$(y_1 - y_A) - \frac{L_1}{2} \sin \psi_1 = 0$$

$$(x_1 + \frac{L_1}{2} \cos \psi_1) - (x_2 - \frac{L_2}{2} \cos \psi_2) = 0$$

$$(y_1 + \frac{L_1}{2} \sin \psi_1) - (y_2 - \frac{L_2}{2} \sin \psi_2) = 0$$

$$\psi_3 - (\psi_2 + \frac{\pi}{2}) = 0$$

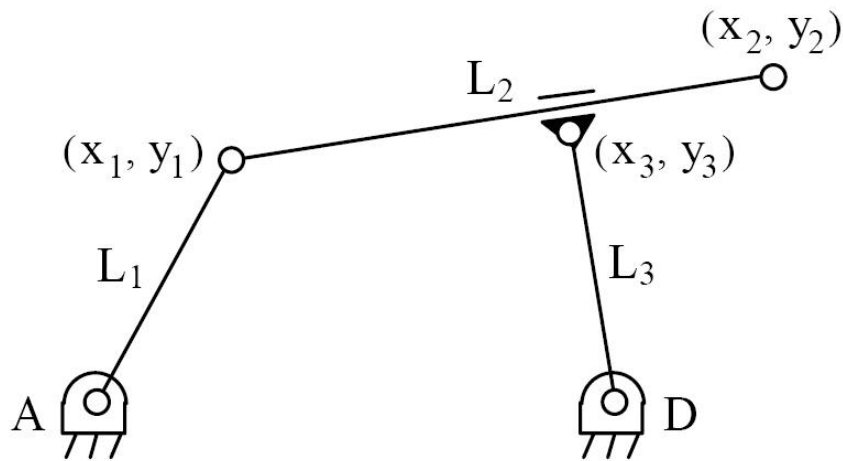
$$(x_2 - x_3) \cos \psi_3 + (y_2 - y_3) \sin \psi_3 - \frac{L_3}{2} = 0$$

$$(x_3 - x_D) - \frac{L_3}{2} \cos \psi_3 = 0$$

$$(y_3 - y_D) - \frac{L_3}{2} \sin \psi_3 = 0$$



Modeling: natural coordinates



$$(x_1 - x_A)^2 + (y_1 - y_A)^2 - L_1^2 = 0$$

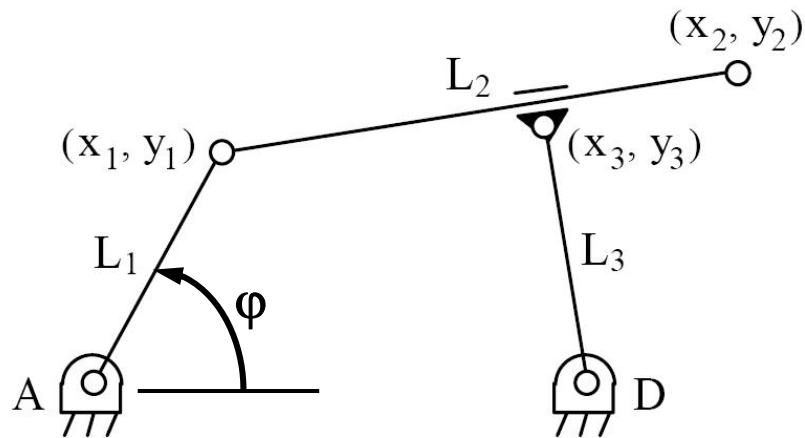
$$(x_2 - x_1)^2 + (y_2 - y_1)^2 - L_2^2 = 0$$

$$(x_3 - x_D)^2 + (y_3 - y_D)^2 - L_3^2 = 0$$

$$(x_2 - x_1)(x_3 - x_D) + (y_2 - y_1)(y_3 - y_D) = 0$$

$$(x_3 - x_1)(y_2 - y_1) - (y_3 - y_1)(x_2 - x_1) = 0$$

Modeling: mixed coordinates (natural + relative)



$$(x_1 - x_A)^2 + (y_1 - y_A)^2 - L_1^2 = 0$$

$$(x_2 - x_1)^2 + (y_2 - y_1)^2 - L_2^2 = 0$$

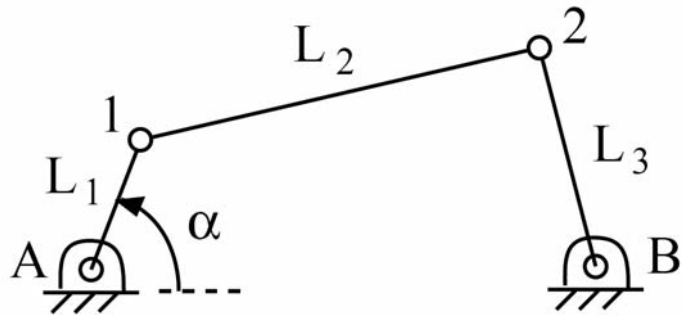
$$(x_3 - x_D)^2 + (y_3 - y_D)^2 - L_3^2 = 0$$

$$(x_2 - x_1)(x_3 - x_D) + (y_2 - y_1)(y_3 - y_D) = 0$$

$$(x_3 - x_1)(y_2 - y_1) - (y_3 - y_1)(x_2 - x_1) = 0$$

$$(x_1 - x_A)(x_D - x_A) + (y_1 - y_A)(y_D - y_A) - L_1 L_4 \cos \phi = 0$$

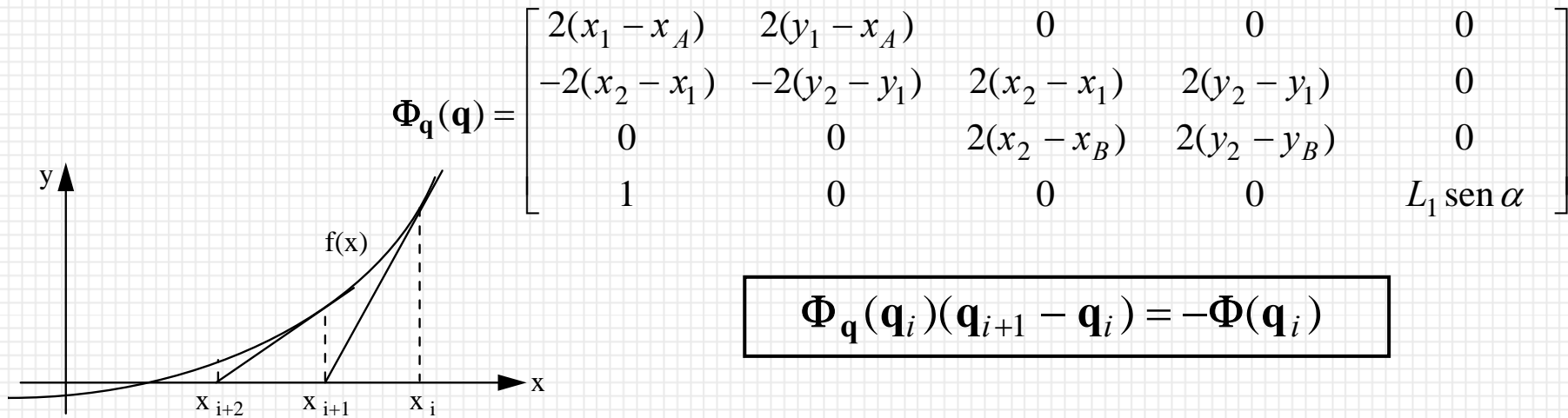
Kinematics: position problem



$$\mathbf{q}^t = \{x_1, y_1, x_2, y_2, \alpha\}$$

$$\left. \begin{aligned} (x_1 - x_A)^2 + (y_1 - y_A)^2 - L_1^2 &= 0 \\ (x_2 - x_1)^2 + (y_2 - y_1)^2 - L_2^2 &= 0 \\ (x_2 - x_B)^2 + (y_2 - y_B)^2 - L_3^2 &= 0 \\ (x_1 - x_A) - L_1 \cos \alpha &= 0 \end{aligned} \right\} \Phi(\mathbf{q}) = 0$$

$$\Phi(\mathbf{q}) \cong \Phi(\mathbf{q}_0) + \Phi_{\mathbf{q}}(\mathbf{q}_0)(\mathbf{q} - \mathbf{q}_0) = 0 \implies \Phi_{\mathbf{q}}(\mathbf{q}_0)(\mathbf{q} - \mathbf{q}_0) = -\Phi(\mathbf{q}_0)$$

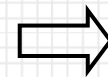


$$\Phi_{\mathbf{q}}(\mathbf{q}_i)(\mathbf{q}_{i+1} - \mathbf{q}_i) = -\Phi(\mathbf{q}_i)$$

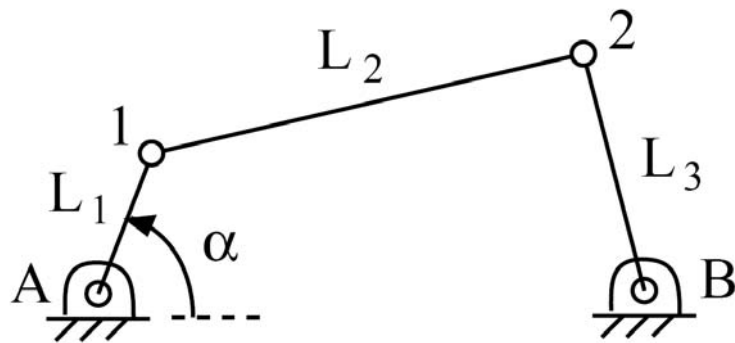
Kinematics: velocity and acceleration problems

$$\Phi(\mathbf{q}) = \mathbf{0} \quad \Rightarrow$$

$$\Phi_{\mathbf{q}}(\mathbf{q})\dot{\mathbf{q}} = \mathbf{0}$$



$$\Phi_{\mathbf{q}}(\mathbf{q})\ddot{\mathbf{q}} = -\dot{\Phi}_{\mathbf{q}}\dot{\mathbf{q}}$$



$$-\dot{\Phi}_{\mathbf{q}}\dot{\mathbf{q}} = \begin{Bmatrix} 2(\dot{x}_1^2 + \dot{y}_1^2) \\ 2[(\dot{x}_2 - \dot{x}_1)^2 + (\dot{y}_2 - \dot{y}_1)^2] \\ 2(\dot{x}_2^2 + \dot{y}_2^2) \\ L_1\dot{\alpha}^2 \cos \alpha \end{Bmatrix}$$

$$\Phi_{\mathbf{q}}(\mathbf{q}) = \begin{bmatrix} 2(x_1 - x_A) & 2(y_1 - x_A) & 0 & 0 & 0 \\ -2(x_2 - x_1) & -2(y_2 - y_1) & 2(x_2 - x_1) & 2(y_2 - y_1) & 0 \\ 0 & 0 & 2(x_2 - x_B) & 2(y_2 - y_B) & 0 \\ 1 & 0 & 0 & 0 & L_1 \sin \alpha \end{bmatrix}$$

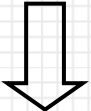
The basic multibody dynamics equations

Lagrange's equations

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{\mathbf{q}}} \right) - \frac{\partial T}{\partial \mathbf{q}} + \Phi_{\mathbf{q}}^t \lambda = \mathbf{Q}$$

Kinetic energy

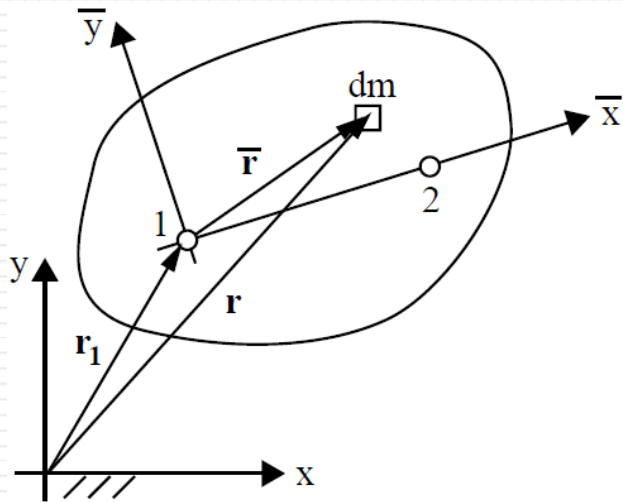
$$T = \frac{1}{2} \dot{\mathbf{q}}^t \mathbf{M} \dot{\mathbf{q}}$$


$$\begin{aligned} \mathbf{M} \ddot{\mathbf{q}} + \Phi_{\mathbf{q}}^t \lambda &= \mathbf{Q} \\ \Phi &= \mathbf{0} \end{aligned}$$

System of differential-algebraic equations (DAE)



Mass matrix



$$\mathbf{r} = \mathbf{r}_1 + \mathbf{A}\bar{\mathbf{r}}$$

$$\mathbf{r}_1 = \begin{Bmatrix} x_1 \\ y_1 \end{Bmatrix}$$

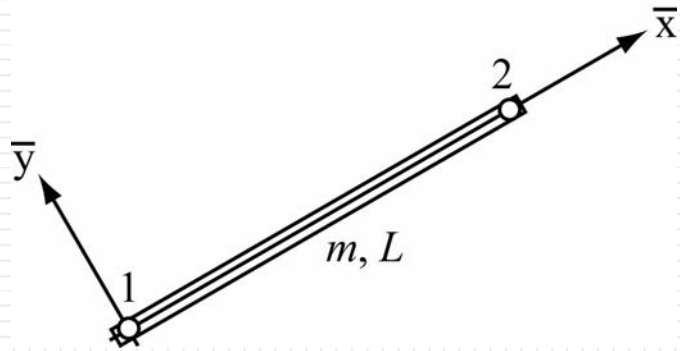
$$\mathbf{A} = \frac{1}{L} \begin{pmatrix} x_2 - x_1 & y_1 - y_2 \\ y_2 - y_1 & x_2 - x_1 \end{pmatrix}$$

$$\dot{\mathbf{r}} = \dot{\mathbf{r}}_1 + \dot{\mathbf{A}}\bar{\mathbf{r}}$$

$$T = \frac{1}{2} \int \dot{\mathbf{r}}^t \dot{\mathbf{r}} dm$$

$$T = \frac{1}{2} \{ \dot{x}_1 \dot{y}_1 \dot{x}_2 \dot{y}_2 \} \begin{bmatrix} m - 2m \frac{\bar{x}_G}{L} + \frac{I_1}{L^2} & 0 & m \frac{\bar{x}_G}{L} - \frac{I_1}{L^2} & -m \frac{\bar{y}_G}{L} \\ 0 & m - 2m \frac{\bar{x}_G}{L} + \frac{I_1}{L^2} & m \frac{\bar{y}_G}{L} & m \frac{\bar{x}_G}{L} - \frac{I_1}{L^2} \\ m \frac{\bar{x}_G}{L} - \frac{I_1}{L^2} & m \frac{\bar{y}_G}{L} & \frac{I_1}{L^2} & 0 \\ -m \frac{\bar{y}_G}{L} & m \frac{\bar{x}_G}{L} - \frac{I_1}{L^2} & 0 & \frac{I_1}{L^2} \end{bmatrix} \begin{Bmatrix} \dot{x}_1 \\ \dot{y}_1 \\ \dot{x}_2 \\ \dot{y}_2 \end{Bmatrix}$$

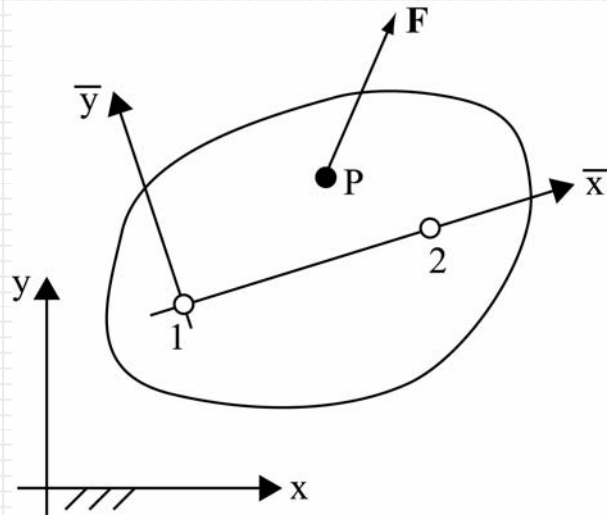
Mass matrix: homogeneous rod



$$\bar{x}_G = \frac{L}{2} \quad ; \quad \bar{y}_G = 0 \quad ; \quad I_1 = \frac{1}{3}mL^2$$

$$\mathbf{M} = \begin{bmatrix} \frac{m}{3} & 0 & \frac{m}{6} & 0 \\ 0 & \frac{m}{3} & 0 & \frac{m}{6} \\ \frac{m}{6} & 0 & \frac{m}{3} & 0 \\ 0 & \frac{m}{6} & 0 & \frac{m}{3} \end{bmatrix}$$

Force vector



$$\mathbf{r}_P = \mathbf{r}_1 + \mathbf{A}\bar{\mathbf{r}}_P$$

$$\mathbf{r}_P = \begin{Bmatrix} x_1 \\ y_1 \end{Bmatrix} + \frac{1}{L} \begin{bmatrix} x_2 - x_1 & y_1 - y_2 \\ y_2 - y_1 & x_2 - x_1 \end{bmatrix} \begin{Bmatrix} \bar{x}_P \\ \bar{y}_P \end{Bmatrix}$$

$$\mathbf{r}_P = \frac{1}{L} \begin{bmatrix} L - \bar{x}_P & \bar{y}_P & \bar{x}_P & -\bar{y}_P \\ -\bar{y}_P & L - \bar{x}_P & \bar{y}_P & \bar{x}_P \end{bmatrix} \begin{Bmatrix} x_1 \\ y_1 \\ x_2 \\ y_2 \end{Bmatrix} = \mathbf{C}_P \mathbf{q}$$

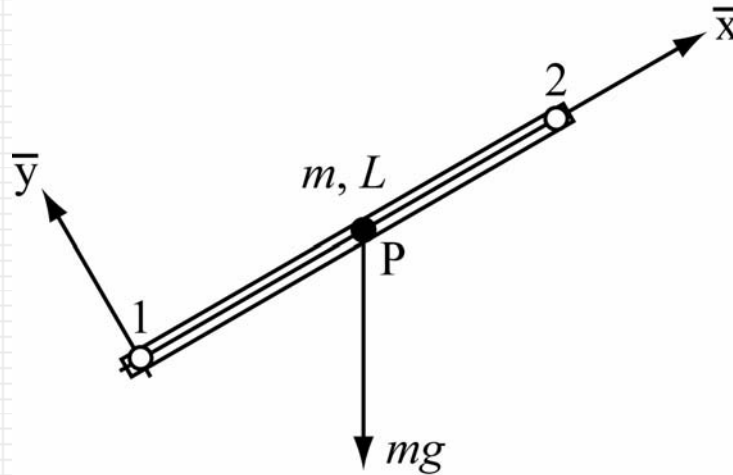
$$\dot{\mathbf{r}}_P = \mathbf{C}_P \dot{\mathbf{q}}$$

$$\dot{\tilde{W}} = \mathbf{F}^t \dot{\tilde{\mathbf{r}}}_P = \mathbf{F}^t \mathbf{C}_P \dot{\tilde{\mathbf{q}}} = \mathbf{Q}^t \dot{\tilde{\mathbf{q}}}$$

$$\mathbf{Q} = \mathbf{C}_P^T \mathbf{F}$$



Force vector: weight acting on homogeneous rod

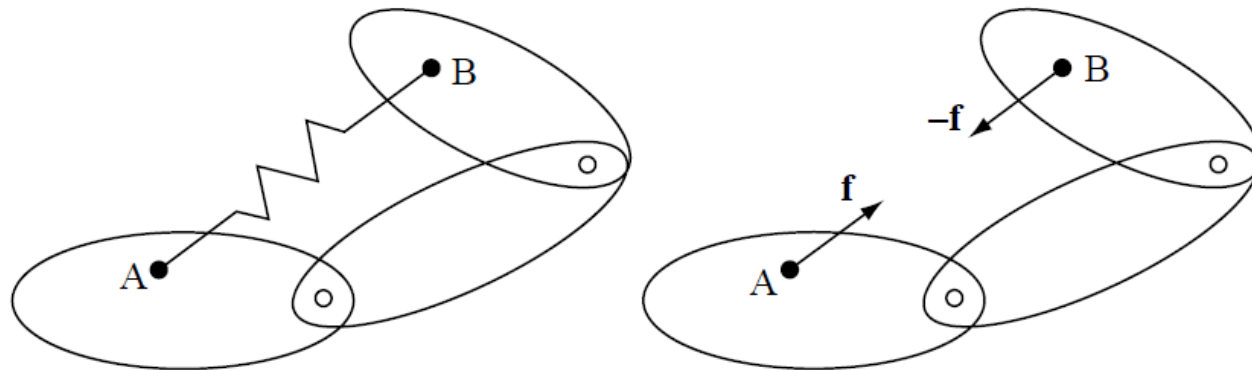


$$\bar{x}_P = \frac{L}{2} \quad ; \quad \bar{y}_P = 0$$

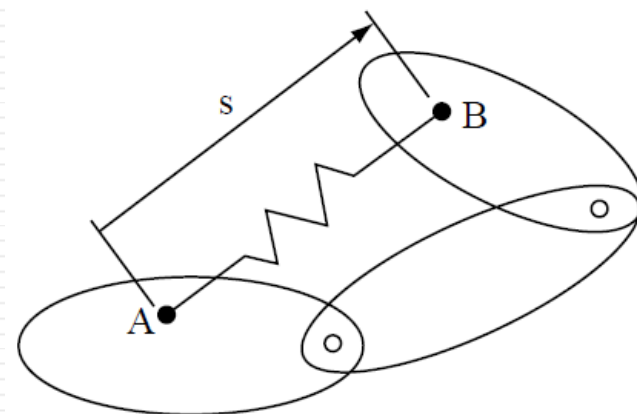
$$\mathbf{C}_P = \begin{bmatrix} \frac{1}{2} & 0 & \frac{1}{2} & 0 \\ 0 & \frac{1}{2} & 0 & \frac{1}{2} \end{bmatrix} \quad ; \quad \mathbf{F} = \begin{Bmatrix} 0 \\ -mg \end{Bmatrix}$$

$$\mathbf{Q} = \begin{Bmatrix} 0 \\ -\frac{mg}{2} \\ 0 \\ -\frac{mg}{2} \end{Bmatrix}$$

Springs, dampers and actuators

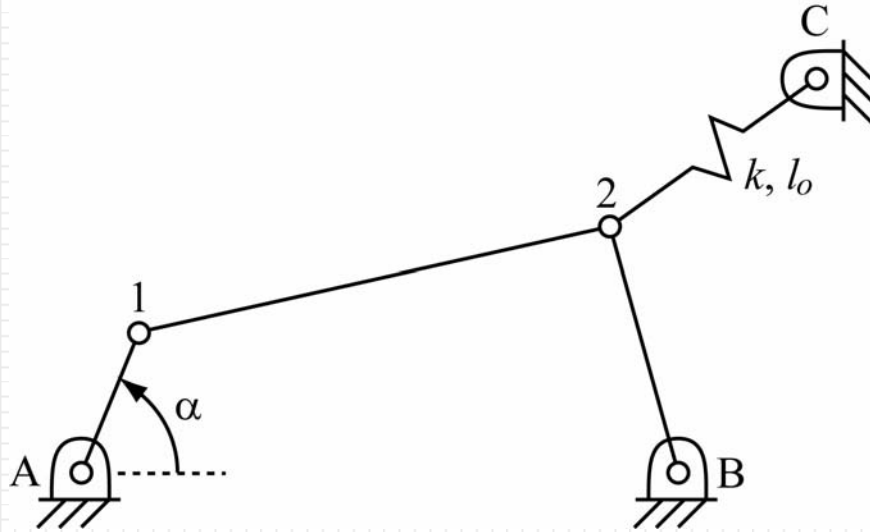


$$\mathbf{f} = -k(d_{AB} - l_o) \frac{\mathbf{r}_A - \mathbf{r}_B}{d_{AB}}$$



$$f = -k(s - l_o)$$

Spring acting on four-bar mechanism



$$\mathbf{q} = \begin{Bmatrix} x_1 \\ y_1 \\ x_2 \\ y_2 \\ \alpha \end{Bmatrix}$$

$$\mathbf{F} = -k(l - l_0) \frac{\mathbf{r}_2 - \mathbf{r}_C}{l} \quad ; \quad l = |\mathbf{r}_2 - \mathbf{r}_C| \quad \Rightarrow \quad \mathbf{Q} = \begin{Bmatrix} 0 \\ 0 \\ F_x \\ F_y \\ 0 \end{Bmatrix}$$

Stabilized Lagrange (Baumgarte)

DAE

$$\begin{aligned} \mathbf{M}\ddot{\mathbf{q}} + \Phi_{\mathbf{q}}^t \lambda &= \mathbf{Q} \\ \Phi &= \mathbf{0} \end{aligned}$$

ODE

$$\begin{cases} \mathbf{M}\ddot{\mathbf{q}} + \Phi_{\mathbf{q}}^t \lambda = \mathbf{Q} \\ \ddot{\Phi} = \mathbf{0} \end{cases} \Rightarrow \begin{bmatrix} \mathbf{M} & \Phi_{\mathbf{q}}^T \\ \Phi_{\mathbf{q}} & \mathbf{0} \end{bmatrix} \begin{Bmatrix} \ddot{\mathbf{q}} \\ \lambda \end{Bmatrix} = \begin{Bmatrix} \mathbf{Q} \\ -\dot{\Phi}_{\mathbf{q}} \dot{\mathbf{q}} \end{Bmatrix}$$

Unstable

$$\begin{cases} \mathbf{M}\ddot{\mathbf{q}} + \Phi_{\mathbf{q}}^t \lambda = \mathbf{Q} \\ \ddot{\Phi} + 2\xi\omega\dot{\Phi} + \omega^2\Phi = \mathbf{0} \end{cases}$$

Stable

$$\begin{bmatrix} \mathbf{M} & \Phi_{\mathbf{q}}^T \\ \Phi_{\mathbf{q}} & \mathbf{0} \end{bmatrix} \begin{Bmatrix} \ddot{\mathbf{q}} \\ \lambda \end{Bmatrix} = \begin{Bmatrix} \mathbf{Q} \\ -\dot{\Phi}_{\mathbf{q}} \dot{\mathbf{q}} - 2\xi\omega\dot{\Phi} - \omega^2\Phi \end{Bmatrix}$$



Penalty

DAE

$$\mathbf{M}\ddot{\mathbf{q}} + \mathbf{\Phi}_q^t \boldsymbol{\lambda} = \mathbf{Q}$$

$$\boldsymbol{\Phi} = \mathbf{0}$$

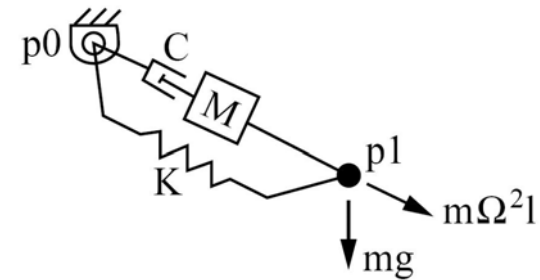
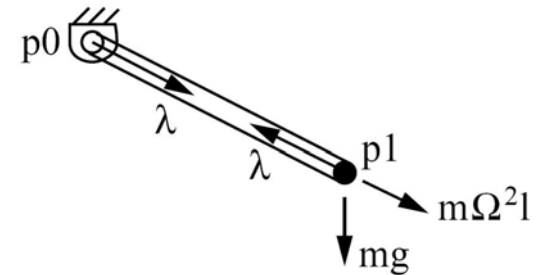
⇒ ODE

Aproximation of
Lagrange
multipliers

$$\boldsymbol{\lambda} = \alpha (\ddot{\boldsymbol{\Phi}} + 2\xi\omega\dot{\boldsymbol{\Phi}} + \omega^2\boldsymbol{\Phi})$$

$$\mathbf{M}\ddot{\mathbf{q}} + \mathbf{\Phi}_q^T \alpha (\ddot{\boldsymbol{\Phi}} + 2\xi\omega\dot{\boldsymbol{\Phi}} + \omega^2\boldsymbol{\Phi}) = \mathbf{Q}$$

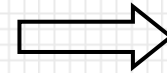
$$(\mathbf{M} + \alpha \mathbf{\Phi}_q^T \mathbf{\Phi}_q) \ddot{\mathbf{q}} = \mathbf{Q} - \alpha \mathbf{\Phi}_q^T (\dot{\boldsymbol{\Phi}}_q \dot{\mathbf{q}} + 2\xi\omega\dot{\boldsymbol{\Phi}} + \omega^2\boldsymbol{\Phi})$$



Velocity transformation: matrix R

DAE

$$\begin{aligned} \mathbf{M}\ddot{\mathbf{q}} + \Phi_{\mathbf{q}}^t \boldsymbol{\lambda} &= \mathbf{Q} \\ \Phi &= \mathbf{0} \end{aligned}$$



ODE

Transformation to
independent
coordinates

$$\begin{cases} \dot{\mathbf{q}} = \mathbf{R}\dot{\mathbf{z}} \\ \ddot{\mathbf{q}} = \mathbf{R}\ddot{\mathbf{z}} + \dot{\mathbf{R}}\dot{\mathbf{z}} \end{cases}$$

$$\begin{cases} \dot{q}_1 \\ \dots \\ \dot{q}_i \\ \dots \\ \dot{q}_n \end{cases} = \begin{bmatrix} R_{11} & \dots & R_{1i} & \dots & R_{1f} \\ \dots & \dots & \dots & \dots & \dots \\ R_{i1} & \dots & R_{ii} & \dots & R_{if} \\ \dots & \dots & \dots & \dots & \dots \\ R_{n1} & \dots & R_{ni} & \dots & R_{nf} \end{bmatrix} \begin{cases} 0 \\ \dots \\ 1 \\ \dots \\ 0 \end{cases}$$

$$\mathbf{R}^T \mathbf{M} \mathbf{R} \ddot{\mathbf{z}} = \mathbf{R}^T (\mathbf{Q} - \mathbf{M} \dot{\mathbf{R}} \dot{\mathbf{z}})$$

$$\bar{\mathbf{M}} \ddot{\mathbf{z}} = \bar{\mathbf{Q}}$$



Numerical integrators

- DAE are converted to ODE.
- Many integrators are available for first order ODE of the form:

$$\dot{\mathbf{y}} = \mathbf{f}(\mathbf{y}, t)$$

- However, the MBD problem is second order, so variables must be duplicated in order to use such integrators:

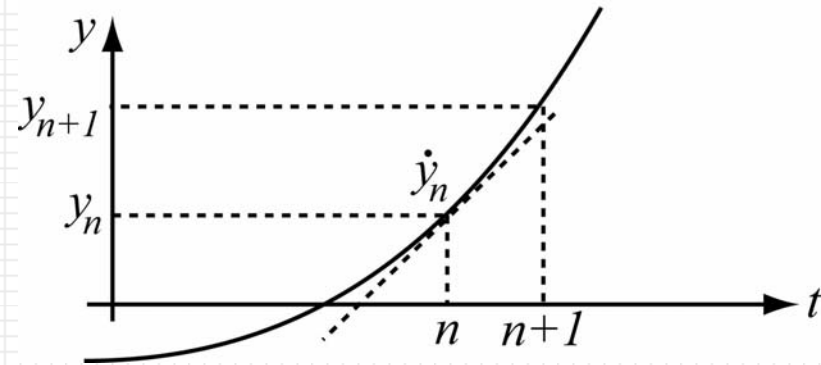
$$\mathbf{y} = \begin{Bmatrix} \mathbf{q} \\ \dot{\mathbf{q}} \end{Bmatrix} \quad \Longrightarrow \quad \dot{\mathbf{y}} = \begin{Bmatrix} \dot{\mathbf{q}} \\ \ddot{\mathbf{q}} \end{Bmatrix}$$

- Properties of integrators: stability and accuracy.
- *Stiff* problems.



Numerical integrators

- Classification of integrators:
 - Single step vs multistep.
 - Fixed step vs variable step.
 - Explicit vs implicit (iteration: fixed point vs Newton-Raphson).



Forward Euler $\mathbf{y}_{n+1} = \mathbf{y}_n + \dot{\mathbf{y}}_n \Delta t$

2nd-order explicit
Runge-Kutta

$$\mathbf{y}_{n+1} = \mathbf{y}_n + \frac{\Delta t}{2} (\dot{\mathbf{y}}_1 + \dot{\mathbf{y}}_2)$$

$$\dot{\mathbf{y}}_1 = \mathbf{f}(\mathbf{y}_n, t)$$

$$\dot{\mathbf{y}}_2 = \mathbf{f}(\mathbf{y}_n + \dot{\mathbf{y}}_1 \Delta t, t + \Delta t)$$

Trapezoidal rule

$$\mathbf{y}_{n+1} = \mathbf{y}_n + \frac{\Delta t}{2} (\dot{\mathbf{y}}_n + \dot{\mathbf{y}}_{n+1})$$

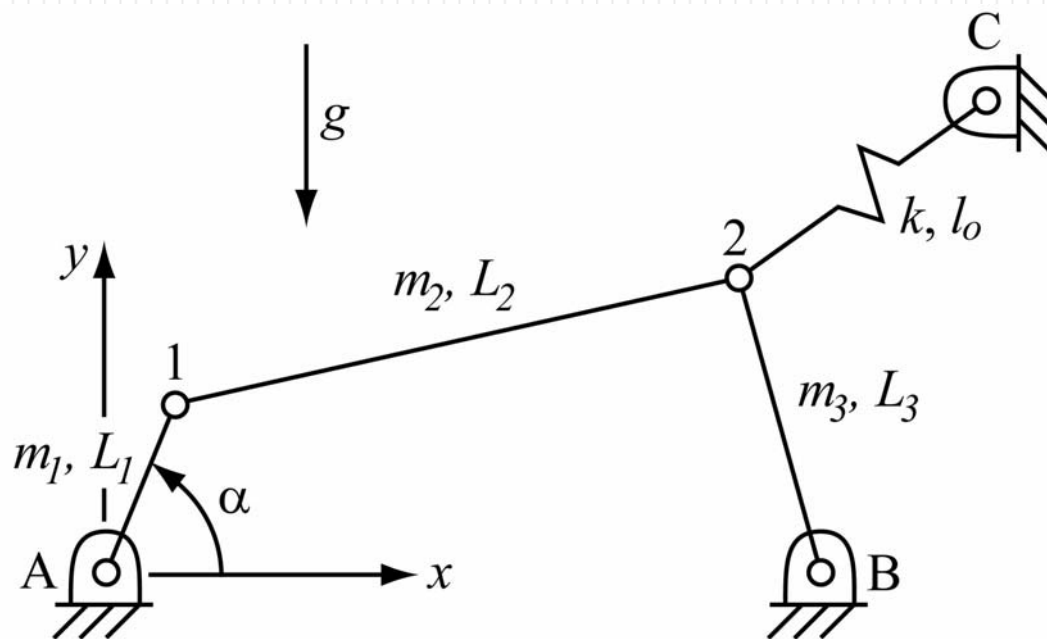
Adams-Bashforth / Adams-Moulton

$$\mathbf{y}_{n+1} = \mathbf{y}_n + \frac{\Delta t}{24} (55\dot{\mathbf{y}}_n - 59\dot{\mathbf{y}}_{n-1} + 37\dot{\mathbf{y}}_{n-2} - 9\dot{\mathbf{y}}_{n-3})$$

$$\mathbf{y}_{n+1} = \mathbf{y}_n + \frac{\Delta t}{24} (9\dot{\mathbf{y}}_{n+1} + 19\dot{\mathbf{y}}_n - 5\dot{\mathbf{y}}_{n-1} + \dot{\mathbf{y}}_{n-2})$$



Example: four-bar mechanism



$$\mathbf{q} = \begin{Bmatrix} x_1 \\ y_1 \\ x_2 \\ y_2 \\ \alpha \end{Bmatrix}$$